(A.1.1)



Solution / marking scheme - Characterizing Soil Colloids (10 points)

General rules

• In the following, "coefficients" refer to the numerical factors and do not include parameters.

Part A. Analysis of motions of colloidal particles (1.6 points)

A.1 (total 0.8 pt)

(0.4 pt)

$$v_0 = \frac{I_0}{M}$$

—— partial points ——

$$(0.2~{\rm pt}) \quad Mv_0 = I_0$$

(0.4 pt)

$$\tau = \frac{M}{\gamma}$$

• 0.4pt if the answers are $v_0=M/\gamma$ and $\tau=I_0/M$.

——— partial points –

$$(0.2 \text{ pt}) \quad M\dot{v} = -\gamma v(t) \tag{A.1.2}$$

A.2 (total 0.8 pt)

(0.6 pt)

$$v(t) = \sum_i \frac{I_i}{M} e^{-(t-t_i)/\tau}$$

- 0.4pt if $\frac{I_i}{M}e^{-(t-t_i)/ au}$ is written. The subscript can be any dummy variable used in the summation symbol.
- 0.2pt if sum is taken (if Σ is written).
- the range of sum is not considered here (even if it is wrong).
- $\tau = M/\gamma$ can be substituted.

(0.2 pt)

the inequality specifying the range of t_i that needs to be considered:

 $0 < t \le t$

- < can be \le (full mark is given).
- 0.2pt (full mark) is given to $t_i < t$ (without 0 <)
- No point is given to $t_i > 0$ solely.



Part B. Effective equation of motion (1.8 points)

B.1 (total 1.0 pt)

(0.5 pt) Usable letters: C, δ, t

$$\langle \Delta x(t) \rangle = 0$$

(0.5 pt) Usable letters: C, δ, t

$$\langle \Delta x(t)^2 \rangle = C \delta t$$

—— partial points -

$$(0.3 \text{ pt}) \quad \Delta x(t) = \sum_{n=1}^{N} v_n \delta \tag{B.1.1} \label{eq:bound}$$

• 0.2pt if δ is missing.

$$(0.2 \text{ pt}) \quad \langle \Delta x(t)^2 \rangle = \sum_{n=1}^{N} C \delta^2 = NC \delta^2 = C \delta t$$
(B.1.2)

• 0.2pt only if $C\delta t$ is written. 0.1pt if only $\sum_{n=1}^{N} C\delta^2$ or $NC\delta^2$ is written.

B.2 (total 0.8 pt)

(0.4 pt)

$$\alpha = -1$$

(0.4 pt)

$$\beta = 1$$



Part C. Electrophoresis (2.7 points)

C.1 (total 0.5 pt)

(0.5 pt) Usable letters: $v, \delta, n(x_0), \frac{dn}{dx}(x_0)$

$$N_{+}(x_{0})=\frac{1}{2}n(x_{0})v-\frac{1}{4}\frac{dn}{dx}(x_{0})v^{2}\delta$$

- 0.3pt if δ or A or both are multiplied unnecessarily (subtraction of 0.2pt)
- 0.4pt if either coefficient (or both) is wrong (subtraction of 0.1pt)
- 0.4pt if the sign of the second term is wrong (subtraction of 0.1pt)
- If more than one of the above mistakes are made, points to subtract accumulate.

——— partial points —

$$(0.3 \text{ pt}) \quad N_+(x_0) = \int_{x_0 - v\delta}^{x_0} \frac{n(x)}{2\delta} dx \qquad \text{or} \qquad N_+(x_0) = \frac{v}{2} n(x_0 - v\delta/2) \tag{C.1.1}$$

- 0.2pt if δ or A or both are multiplied unnecessarily (subtraction of 0.1pt)
- 0.2pt if any coefficient is wrong (subtraction of 0.1pt)
- 0.2pt if the integration range is $\int_{x_0}^{x_0+v\delta}$ (subtraction of 0.1pt)
- If more than one of the above mistakes are made, points to subtract accumulate.

C.2 (total 0.7 pt)

(0.4 pt) Usable letters: $C, \delta, n(x_0), \frac{dn}{dx}(x_0)$

$$J_D(x) = -\frac{1}{2}\frac{dn}{dx}(x)C\delta$$

• 0.3pt if the sign or the coefficient is wrong (but pay attention to carryover from C.1).

– partial points -

$$(0.1 \ \mathrm{pt}) \quad N_{-}(x_0) = \frac{1}{2} n(x_0) v + \frac{1}{4} \frac{dn}{dx}(x_0) v^2 \delta \tag{C.2.1}$$

(0.1 pt) Usable letters: C, δ

$$D = \frac{1}{2}C\delta$$

(0.2 pt) Usable letters: D, t

$$\langle \Delta x(t)^2 \rangle = 2Dt$$

• No point if the answer includes C or δ .



C.3 (total 0.5 pt)

(0.5 pt) Usable letters: n(x), T, Q, E, k

$$\frac{dn}{dx} = \frac{n(x)}{kT}QE$$

——— partial points ———

$$(0.3 \text{ pt}) \quad \Pi(x)A + n(x)A\Delta x QE = \Pi(x + \Delta x)A \tag{C.3.1}$$

C.4 (total 0.5 pt)

(0.3 pt)

$$\langle v(t)\rangle = \frac{QE}{\gamma}(1-e^{-t/\tau})$$

• $\tau = M/\gamma$ can be substituted.

——— partial points ———

(0.3 pt)
$$M \frac{d\langle v(t)\rangle}{dt} = -\gamma \langle v(t)\rangle + QE$$
 (C.4.1)

(0.2 pt)

$$u = \frac{QE}{\gamma}$$

C.5 (total 0.5 pt)

($0.5~\mathrm{pt}$) Usable letters: k,γ,T

$$D = \frac{kT}{\gamma}$$

—— partial points -

$$(0.2~{\rm pt}) \quad J_D(x) = -\frac{DQE}{kT} n(x)$$

(C.5.1)

$$(0.2 \; \mathrm{pt}) \quad J_Q(x) = \frac{QE}{\gamma} n(x)$$

(C.5.2)



Part D. Mean square displacement (2.4 points)

D.1 (total 1.0 pt)

(1.0 pt)

 $N_A = 5.6 \times 10^{23} \; \mathrm{mol^{-1}}$

- No reduction if the unit is missing.
- 0.8pt if the second digit is wrong but the value is in the range 5.5– 5.7×10^{23} .

——— partial points -

$$(0.5 \text{ pt}) \quad \langle \Delta x^2 \rangle = \frac{RT\Delta t}{3\pi a \eta N_A} \tag{D.1.1}$$

- 0.3pt if both the answer of C.2 ($\langle \Delta x^2 \rangle = 2D\Delta t$) and that of C.5 ($D = \frac{kT}{\gamma}$) are given in the worksheet for D.1. The combination of them ($\langle \Delta x^2 \rangle = \frac{2kT\Delta t}{\gamma}$) is also acceptable. $k = R/N_A$ and $\gamma = 6\pi a \eta$ can be substituted here.
- No reduction if t is used for Δt .

(0.3 pt)
$$\langle \Delta x^2 \rangle = 6.34 \,\mu\text{m}^2$$
 (D.1.2)

- No reduction if the value is in the range 6.2–6.4 μ m².
- 0.2pt if the value is in the range 4–9 $\mu \rm m^2$ or if the standard deviation of Δx is in the range 2–3 $\mu \rm m$.
- Subtract 0.1pt if the unit is missing or wrong.



D.2 (total 0.8 pt)

(0.2 pt) Usable letters: u, D, t

$$\langle \Delta x^2 \rangle = (ut)^2 + 2Dt$$

(0.2 pt)

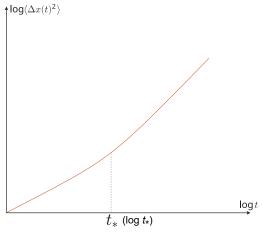
$$\langle \Delta x^2 \rangle \propto egin{cases} t & ext{for small } t \\ t^2 & ext{for large } t \end{cases}$$
• 0.1pt independently for each answer.

(0.2 pt)

$$t_* = \frac{2D}{u^2}$$

(0.2 pt)

Points are given according to the criteria given below.



- 0.1pt if the graph is monotonically increasing and convex (no points if there are multiple curves that look like the answered graph)
- 0.1pt if t_* is written between the two power-law regions (the label can be either t_* or $\log t_*$).

D.3 (total 0.6 pt)

(0.6 pt)

$$\langle \Delta x^2 \rangle = \begin{cases} 2Dt & \text{for small } t \\ u_0^2 t^2 & \text{for intermediate } t \\ (u_0^2 \delta)t & \text{for large } t \end{cases}$$

- 0.2pt independently for each answer.
- Wrong answer in B.1 is not considered.



Part E. Water purification (1.5 points)

E.1 (total 1.5 pt)

(1.5 pt)

$$c=\frac{8B^2\epsilon^3(kT)^5}{e^4N_AA^2q^6}$$

• 1.3pt if only the coefficient is wrong (e is a part of the coefficient) (then no further partial point is given)

——— partial points —

(0.5 pt)
$$\min U'(d) = 0$$
 (E.1.1)

- No point for U'(d) = 0 solely (without indicating what d to consider) or U'(a) = 0.
- 0.2pt if the graph of the potential with an energy barrier (the graph first increases monotonically, then decreases monotonically) is drawn (this is the potential for $c < c_*$)
- independently, 0.2pt if the graph of the potential without an energy barrier (the graph increases monotonically) is drawn (this is the potential for $c > c_*$)

(0.2 pt)
$$U'(d) = \frac{A}{d^2} - \frac{B\epsilon(kT)^2}{q^2\lambda} e^{-d/\lambda} = 0$$
 (E.1.2)

(0.2 pt)
$$U''(d) = -\frac{2A}{d^3} + \frac{B\epsilon(kT)^2}{g^2\lambda^2}e^{-d/\lambda} = 0$$
 (E.1.3)

• 0.2pt (out of the 0.4pt right above) if both U'(d) = 0 and U''(d) = 0 are written as simultaneous equations, without their correct explicit forms.

(0.2 pt)
$$d = 2\lambda = \sqrt{\frac{Aq^2\lambda}{B\epsilon(kT)^2}}$$
 (E.1.4)

(0.3 pt)
$$\lambda = \frac{e^2 A q^2}{4B\epsilon (kT)^2}$$
 (E.1.5)

- 1.4pt is given in total if (E.1.5) is written.
- 1.2pt if only the coefficient is wrong (*e* is a part of the coefficient)



E.1 (cont.)

Another solution: it is also physically reasonable to consider $\max U(d)=0$ instead of (E.1.1), though this does not meet the requirements given in the question. Therefore, partial points may be given as follows if the question is answered along this line.

– partial points –

(0.5 pt)
$$\max U(d) = 0$$
 (E.1.6)

- No point for U(d) = 0 solely (without indicating what d to consider) or U(a) = 0.
- 0.2pt if the graph of the potential with an energy barrier that is higher than U=0 or $U(d\to\infty)$ is drawn (this is the potential for $c< c_*$)
- independently, 0.2pt if the graph of the potential with an energy barrier that is lower than U=0 or $U(d\to\infty)$ is drawn (this is the potential for $c>c_*$)

$$U(d) = -\frac{A}{d} + \frac{B\epsilon(kT)^2}{q^2}e^{-d/\lambda} = 0$$
 (E.1.7)

(0.2 pt)
$$U'(d) = \frac{A}{d^2} - \frac{B\epsilon(kT)^2}{q^2\lambda} e^{-d/\lambda} = 0$$
 (E.1.8)

- No point for (E.1.7)
- 0.2pt if both U(d) = 0 are U'(d) = 0 are written as simultaneous equations

(0.5 pt)
$$d = \lambda = \frac{eAq^2}{B\epsilon(kT)^2}$$
 (E.1.9)

- 1.2pt is given in total if (E.1.9) is written.
- 1.0pt if only the coefficient is wrong (e is a part of the coefficient)

(0.1 pt)
$$c = \frac{B^2 \epsilon^3 (kT)^5}{2e^2 N_A A^2 q^6}$$
 (E.1.10)

- 1.3pt is given in total if (E.1.10) is written.
- 1.1pt if only the coefficient is wrong (e is a part of the coefficient)



Solution / marking scheme - Neutron Stars (10 points)

General rules

• In the following, "coefficients" refer to the numerical factors and do not include parameters.

Part A. Mass and stability of nuclei (2.5 points)

A.1 (total 0.9 pt)

(0.9 pt)

A = 50

- No reduction if $A = 5.0 \times 10^1$.
- 0.8 pt if the value is in the range 49.5–50.4.

— partial points –

$$(0.2 \text{ pt}) \quad \frac{B}{A} = a_V - a_S A^{-1/3} - \frac{a_C}{4} A^{2/3} \tag{A.1.1}$$

ullet No reduction if the difference from (A.1.1) is only the overall coefficient. This rule is applied throughout.

(0.1 pt)
$$\frac{d(B/A)}{dA} = 0$$
 (A.1.2)

(0.2 pt)
$$\frac{a_S}{3}A^{-4/3} - \frac{a_C}{6}A^{-1/3} = 0$$
 (A.1.3)

• Points for (A.1.2) are given if (A.1.3) is stated although (A.1.2) is not explicitly written.

(0.2 pt)
$$A = \frac{2a_S}{a_C}$$
 (A.1.4)

ullet 0.7 pt is given if the correct expression for A appears even if the intermediate steps are not fully written.



A.2 (total 0.9 pt)

(0.9 pt)

 $Z^* = 79$

- No reduction if $Z^* = 78$.
- 0.8 pt if the value is in the range 77.5–79.4.

— partial points —

$$(0.3 \text{ pt}) \quad -2a_C \frac{Z^*}{A^{1/3}} - 4a_{\text{sym}} \frac{2Z^* - A}{A} = 0 \tag{A.2.1}$$

(0.4 pt)
$$Z^* = \frac{1}{1 + \frac{a_C}{4a_{\text{sym}}} A^{2/3}} \cdot \frac{A}{2}$$
 (A.2.2)

• No reduction if $a_C/4a_{\mathrm{sym}}$ is replaced by the numerical value in the range 0.007–0.008.

A.3 (total 0.7 pt)

(0.7 pt)

 $C_{\mathrm{fission}} = 0.70$

• No reduction if $C_{\text{fission}} = 0.7$.

· partial points

$$(0.3 \text{ pt}) \quad a_S \left[A^{2/3} - 2 \left(\frac{A}{2} \right)^{2/3} \right] + a_C \left[\frac{Z^2}{A^{1/3}} - 2 \frac{(Z/2)^2}{(A/2)^{1/3}} \right] > 0 \tag{A.3.1}$$

• No point if a_V is not canceled.

$$(0.2 \text{ pt}) \quad \frac{Z^2}{A} > \frac{2^{1/3} - 1}{1 - 2^{-2/3}} \cdot \frac{a_S}{a_C} \tag{A.3.2}$$

- Points for (A.3.1) are given if (A.3.2) is stated although (A.3.1) is not explicitly written.
- The coefficient may have different expressions, e.g., with $x=2^{1/3}$,

$$\frac{x-1}{1-x^{-2}} = \frac{x^2}{1+x} = \frac{x}{1+x^{-1}} = \dots = 0.702414...$$



Part B. Neutron star as a gigantic nucleus (1.5 points)

B.1 (total 1.5 pt)

(0.8 pt)

 $a_{\rm grav}=6\times 10^{-37}~{\rm MeV}$

- No reduction if the unit is not written.
- 0.7 pt if only the order of magnitude is correct.

———partial points —

(0.4 pt)
$$a_{\text{grav}} = \frac{3}{5} \frac{Gm_N^2}{R_0}$$
 (B.1.1)

(0.2 pt)
$$a_{\text{grav}} = \frac{3}{5} \frac{\hbar c m_N^2}{R_0 M_P^2}$$
 (B.1.2)

- Points for (B.1.1) are given if (B.1.2) is stated although (B.1.1) is not explicitly written.
- No reduction if \hbar is mistyped.

(0.7 pt)

$$A_c = 4\times 10^{55}$$

- No reduction for $A_c = 5 \times 10^{55}$.
- 0.6 pt if only the order of magnitude is correct.

———— partial points —

$$(0.2 \ \mathrm{pt}) \quad a_V A - a_{\mathrm{sym}} A + a_{\mathrm{grav}} A^{5/3} > 0 \tag{B.1.3}$$

(0.3 pt)
$$A_c = \left(\frac{a_{\text{sym}} - a_V}{a_{\text{grav}}}\right)^{3/2}$$
 (B.1.4)

• Points for (B.1.3) are given if (B.1.4) is stated although (B.1.3) is not explicitly written.



Part C. Neutron star in a binary system (6.0 points)

C.1 (total 1.0 pt)

(1.0 pt)

$$\Delta \tau_{\rm II} = \left(1 - \frac{\Delta \phi}{c^2}\right) \Delta \tau_{\rm I}$$

• No points if the coefficient is wrong

partial points -

(0.3 pt)
$$v^2 = 2g\Delta h = 2\Delta\phi$$
 or $v = \sqrt{2\Delta\phi}$ (C.1.1)

(0.5 pt)
$$\Delta \tau_{\rm II} = \sqrt{1 - v^2/c^2} \Delta \tau_{\rm I}$$
 or $\Delta \tau_{\rm II} = \sqrt{1 - 2\frac{\Delta \phi}{c^2}} \Delta \tau_{\rm I}$ (C.1.2)

• Points for (C.1.1) are given if (C.1.2) is stated although (C.1.1) is not explicitly written.

C.2 (total 1.8 pt)

(1.8 pt)

$$\Delta t = \frac{2GM_{\rm WD}}{c^3} \log \left(\frac{4|x_N|x_E}{d^2} \right)$$

- No reduction if 4 is missing in log.
- No reduction if $|x_N|$ is written as $-x_N$.
- 0.1 pt is subtracted if the modulus in $|x_N|$ is missing.
- No points if other coefficients are wrong.

- partial points

$$(0.5 \text{ pt}) \quad t_{\text{E-N}} = \int_{x_{\text{N}}}^{x_{\text{E}}} \frac{dx}{c_{\text{eff}}(x)} \quad \text{or} \quad \Delta t_{\text{E-N}} = \frac{\Delta x}{c_{\text{eff}}(x)}$$

$$(C.2.1)$$

(0.4 pt)
$$t_{\text{E-N}} \simeq \frac{1}{c} \int_{x_N}^{x_E} dx \left(1 + \frac{2GM_{\text{WD}}}{c^2 \sqrt{x^2 + d^2}} \right)$$
 (C.2.2)

• 0.1 pt is subtracted if the coefficient is wrong.

(0.3 pt)
$$\Delta t = \frac{2GM_{\text{WD}}}{c^3} \int_{x_N}^{x_E} \frac{dx}{\sqrt{x^2 + d^2}}$$
 (C.2.3)

$$(0.3~{\rm pt}) \quad \text{Inside the logarithm: } \sqrt{x_N^2+d^2}+x_N\simeq \frac{d^2}{2|x_N|} \text{ and } \sqrt{x_E^2+d^2}-x_E\simeq \frac{d^2}{2x_E} \quad (\text{C.2.4})$$



C.3 (total 1.8 pt)

(1.8 pt)

$$\begin{split} \Delta t_{\rm max} - \Delta t_{\rm min} &= \frac{2GM_{\rm WD}}{c^3} \log(4/\varepsilon^2) \\ \bullet & \text{ No reduction if log is written as ln.} \end{split}$$

partial points -

$$(0.6 \text{ pt}) \quad \Delta t_{\text{max}} = \frac{2GM_{\text{WD}}}{c^3} \log(4x_E/L\varepsilon^2) \tag{C.3.1}$$

- No subtraction points if the factor in log is different but consistent with that in C.2.
- 0.1 pt is subtracted if the coefficient is wrong.

(0.2 pt) Because of
$$x_N > 0$$
 the approx. in log is changed: $x_N + \sqrt{x_N^2 + d^2} \simeq 2L$ (C.3.2)

(0.4 pt)
$$\Delta t_{\min} = \frac{2GM_{\text{WD}}}{c^3} \ln(x_E/L)$$
 (C.3.3)

- Points for (C.3.2) are given if (C.3.3) is stated although (C.3.2) is not explicitly written.
- 0.1 pt is subtracted if the coefficient is wrong.

(0.3 pt) Points are given if
$$L$$
 and x_E dependence is canceled in log. (C.3.4)

C.4 (total 0.8 pt)

(0.8 pt)

$$M_{\rm WD}/M_{\odot}=0.5$$

• No reduction if the value is in the range 0.4-0.5.

—— partial points –

(0.2 pt)
$$\varepsilon^2 \simeq 2 \times (1 - 0.99989) = 0.00022$$
 (C.4.1)

(0.2 pt) From the given graph,
$$\Delta t_{\rm max} - \Delta t_{\rm min} \approx 50\,\mu{\rm s}$$
 (C.4.2)

• No reduction if the value from the graph is in the range $40-50 \,\mu s$.

(0.2 pt)
$$M_{\rm WD}/M_{\odot} \simeq 5/\ln(4/\varepsilon^2)$$
 (C.4.3)

• No reduction if the numerator is in the range 4-5.



C.5 (total 0.4 pt)

(0.4 pt)

$$p=-rac{3}{2}$$
 or -1.5
• No points if the sign is wrong.

—— partial points —

$$(0.3 \text{ pt})$$
 $R^3\omega^2 = (\text{const.})$

(C.5.1)

C.6 (total 0.2 pt)

(0.2 pt)

The most appropriate profile is (b).



Solution / marking scheme - Water and Objects (10 pt)

General rules

• In the following, "coefficients" refer to the numerical factors and do not include parameters.

Part A. Merger of water drops (2.0 pt)

A.1 (total 2.0 pt)

(2.0 pt)

v = 0.23 m/s

• No deduction if the answer falls within the range $0.22 \text{ m/s} \le v \le 0.24 \text{ m/s}$

— partial points —

The surface energy per drop before the merger:

(0.4 pt)
$$E = 4\pi a^2 \gamma$$
 (A.1.1)

The surface energy difference:

(0.6 pt)
$$\Delta E = 4\pi \left(2 - 2^{2/3}\right) a^2 \gamma$$
 (A.1.2)

The transfer of surface energy to kinetic energy:

(0.4 pt)
$$Mv^2/2 = k\Delta E$$
 (A.1.3)

where $M=4\pi a^3\rho/3\times 2=8\pi a^3\rho/3$ is the mass of the drop after the merger.

• No partial point will be given if the factor k is missing.

Numerical evaluation:

$$v = \sqrt{\frac{2k\Delta E}{M}} = \sqrt{3\left(2 - 2^{2/3}\right)\frac{k\gamma}{\rho a}} = \sqrt{3\left(2 - 2^{2/3}\right) \times \frac{0.06 \times (7.27 \times 10^{-2})}{(1.0 \times 10^3) \times (100 \times 10^{-6})}} = 0.23\cancel{2} \text{ m/s}$$



Part B. A vertically placed board (4.5 pt)

B.1 (total 0.6 pt)

Usable letters: ρ, g, z, P_0

(0.6 pt)

$$P=P_0-\rho gz$$

• No point will be given for $P = P_0 + \rho gz$

———— Commentary —

The expression, $P = P_0 - \rho gz$, holds for both z < 0 and z > 0, as long as z is inside the water.

B.2 (total 0.8 pt)

Usable letters: ρ, g, z_1, z_2

(0.8 pt)

$$f_x = \frac{1}{2} \rho g \left(z_2^2 - z_1^2\right)$$

- Give 0.6 pt for $f_x = \rho g \, (z_2^2 - z_1^2)$
- • Give 0.4 pt for $f_x = \frac{1}{2} \rho g \left(z_1^2 - z_2^2\right)$

Commentary -

Because the atmospheric pressure P_0 exerts no net horizontal force on the water block, we have

$$f_{x}=\int_{z_{2}}^{z_{1}}(-\rho gz)dz=\frac{1}{2}\rho g\left(z_{2}^{2}-z_{1}^{2}\right)$$

B.3 (total 0.8 pt)

Usable letters: $\gamma, \theta_1, \theta_2$

(0.8 pt)

$$f_x = \gamma \cos \theta_1 - \gamma \cos \theta_2$$

- Give 0.6 pt for $f_x = \gamma \cos \theta_2 \gamma \cos \theta_1$
- Give 0.4 pt for $f_x=\gamma\cos\theta_2+\gamma\cos\theta_1$ or $f_x=-\gamma\cos\theta_2-\gamma\cos\theta_1.$



B.4 (total 0.8 pt)

(0.4 pt)

a=2

• No point will be given for $a \neq 2$.

Usable letters: γ, ρ

(0.4 pt)

$$\ell = \sqrt{\frac{\gamma}{\rho g}}$$

• If an unnecessary coefficient is included as a factor, 0.2 pt will be deducted.

B.5 (total 1.5 pt)

Usable letters: $\tan \theta_0, \ell$

(1.5 pt)

$$z\left(x\right)=-\ell\tan\theta_{0}e^{-x/\ell}$$

• Deduct 0.2 pt for $z\left(x\right)=-\ell\sin\theta_{0}e^{-x/\ell}$ or $z\left(x\right)=-\ell\theta_{0}e^{-x/\ell}.$

——— partial points ——

 $z' = \tan \theta$ leads to

(0.2 pt)
$$\cos \theta = \frac{1}{\sqrt{1 + (z')^2}}$$
 (B.5.1)

(0.1 pt)
$$\cos \theta \simeq 1 - \frac{1}{2}(z')^2$$
 (B.5.2)

Plug this into Eq.(1) to obtain,

(0.2 pt)
$$\frac{z^2}{\ell^2} - z'^2 = \text{const.}$$
 (B.5.3)

Take the derivative of both sides with respect to x:

(0.5 pt)
$$z'' = \frac{z}{\ell^2}$$
 (B.5.4)

which is the differential equation which determines the water surface form.

General solution:

(0.2 pt)
$$z = Ae^{x/\ell} + Be^{-x/\ell}$$
 (B.5.5)

The boundary condition, $z(\infty) = 0$, leads to

(0.1 pt)
$$A = 0$$
 (B.5.6)

The boundary condition, $z'(0) = \tan \theta_0$, leads to

$$(0.2 \text{ pt}) \quad B = -\ell \tan \theta_0 \tag{B.5.7}$$



Part C. Interaction between two rods (3.5 pt)

C.1 (total 1.0 pt)

Usable letters: $\theta_{\rm a}, \theta_{\rm b}, z_{\rm a}, z_{\rm b}, \rho, g, \gamma$

(1.0 pt)

$$F_{x}=\frac{1}{2}\rho g\left(z_{\mathrm{b}}^{2}-z_{\mathrm{a}}^{2}\right)+\gamma\left(\cos\theta_{\mathrm{b}}-\cos\theta_{\mathrm{a}}\right)$$

- Give 0.8 pt for $F_x = \frac{1}{2} \rho g \left(z_{\rm b}^2 z_{\rm a}^2\right) + \gamma \left(\cos\theta_{\rm a} \cos\theta_{\rm b}\right)$
- $\bullet \ \ \text{Give 0.6 pt for} \ F_x = \frac{1}{2} \rho g \left(z_{\mathrm{b}}^2 z_{\mathrm{a}}^2 \right) + \gamma \cos \theta_2 + \gamma \cos \theta_1 \ \text{or} \ F_x = \frac{1}{2} \rho g \left(z_{\mathrm{b}}^2 z_{\mathrm{a}}^2 \right) \gamma \cos \theta_2 \gamma \cos \theta_1 .$

——— partial points —

The holizontal component of the force due to the pressure is

(0.6 pt)
$$\int_{z_{-}}^{z_{b}} (\rho g z) dz = \frac{1}{2} \rho g \left(z_{b}^{2} - z_{a}^{2} \right)$$
 (C.1.1)

- Commentary —

Comment 1: How to apply the experience in B.1 is as follows. Let $z_{\rm bottom}$ the z-coordinate at the bottom of the rod, then from the discussion in B1, we see

$$F_x = \int_{z_{\rm bottom}}^{z_{\rm a}} (-\rho gz) dz + \left(-\int_{z_{\rm bottom}}^{z_{\rm b}} (-\rho gz) dz\right) = \int_{z_{\rm a}}^{z_{\rm b}} (\rho gz) dz$$

Comment 2: The fact that the contribution due to the pressure does not depend on the shape of the cross-section can be demonstrated as follows. The pressure at the point s on the contour C along the cross-sectional boundary is

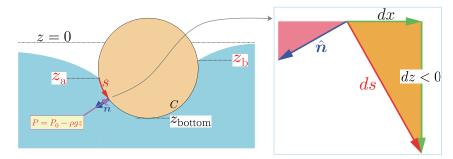
$$-P\hat{n}ds=(-P_0{\color{red}+}\rho g)\hat{n}ds.$$

Let \hat{x} the unit vector pointing the positive x-direction and noting $\hat{x} \cdot \hat{n} ds = dz$ (see the figure shown below), the holizontal component becomes and its holizontal component becomes

$$-P\hat{n}\cdot\hat{x}ds = -P_0dz + \rho qdz.$$

Integrating along the contour C, we obtain

$$\oint_C (-P\hat{n}\cdot\hat{x}ds) = \int_{z_{\rm a}}^{z_{\rm b}} (\rho gz)dz = \frac{1}{2}\rho g\left(z_{\rm b}^2 - z_{\rm a}^2\right)$$





C.2 (total 1.5 pt)

<u>Unusable</u> letters: $\theta_{\rm a}, \theta_{\rm b}, z_{\rm a}, z_{\rm b}$

(1.5 pt)

$$F_x = -\frac{1}{2}\rho g z_0^2$$

- Give 1.3 pt for $F_x = -\rho g z_0^2$.
- Give 0.8 pt for $F_x = \frac{1}{2}\rho g z_0^2$.

—— partial points —

Apply the boundary conditions to Eq. (1) to obtain

(0.6 pt)
$$\underbrace{\frac{1}{2}\rho g z_{\rm a}^2 + \gamma \cos \theta_{\rm a}}_{x=x_{\rm a}} = \underbrace{\frac{1}{2}\rho g z_{\rm 0}^2 + \gamma}_{x=0}$$
 (C.2.1)

• Give 0.4 pt for $\rho g z_{\rm a}^2 + \gamma \cos \theta_{\rm a} = \rho g z_0^2 + \gamma$

$$(0.6 \text{ pt}) \quad \underbrace{\frac{1}{2}\rho g z_b^2 + \gamma \cos \theta_b}_{x=x_b} = \underbrace{\gamma}_{x\to\infty}$$
(C.2.2)

• Give 0.4 pt for $\rho g z_{\rm b}^2 + \gamma \cos\theta_{\rm b} = \rho g z_0^2$ F_x is obtained by subtracting (C2.1) from (C2.2).



C.3 (total 1.0 pt)

Usable letters: $x_{\rm a}, z_{\rm a}$

(1.0 pt)

$$z_0 = \frac{2z_{\mathrm{a}}}{e^{x_{\mathrm{a}}/\ell} + e^{-x_{\mathrm{a}}/\ell}}$$

 • Correct alternative answer:
$$z_0 = \frac{z_{\rm a}}{\cosh(x_{\rm a}/\ell)} = z_{\rm a} {\rm sech}(x_{\rm a}/\ell)$$

— partial points -

General solution: $z(x) = Ae^{x/\ell} + Be^{-x/\ell}$

Taking into account the left-right symmetry, we obtain,

(0.3 pt)
$$A = B$$
 (C.3.1)

Boundary condition, $z(0) = z_0$ leads to

(0.3 pt)
$$A + B = z_0$$
 (C.3.2)

Find the coefficients:

(0.2 pt)
$$A = z_0/2$$
 (C.3.3)

(0.2 pt)
$$B = z_0/2$$
 (C.3.4)